

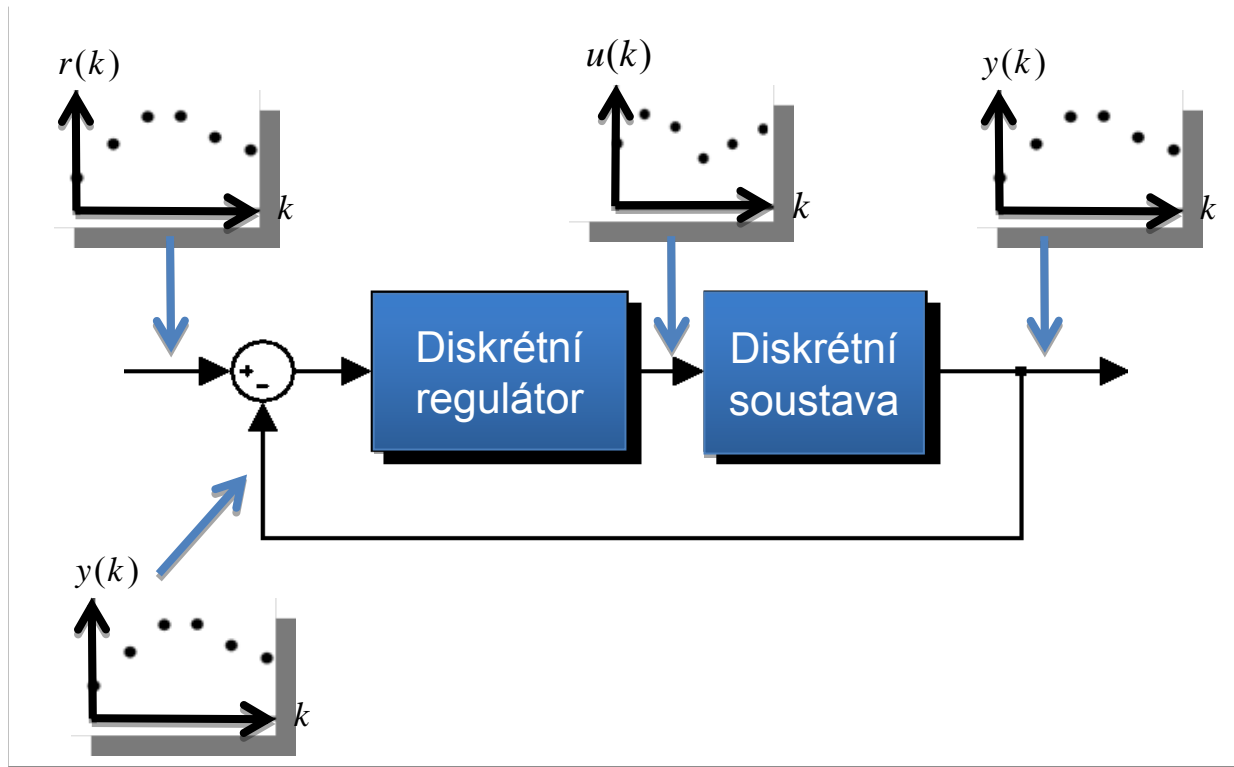
Digital control.
Sampling and reconstruction.
Sampled data systems.



Martin Hromcik.
Automatic Control 2012



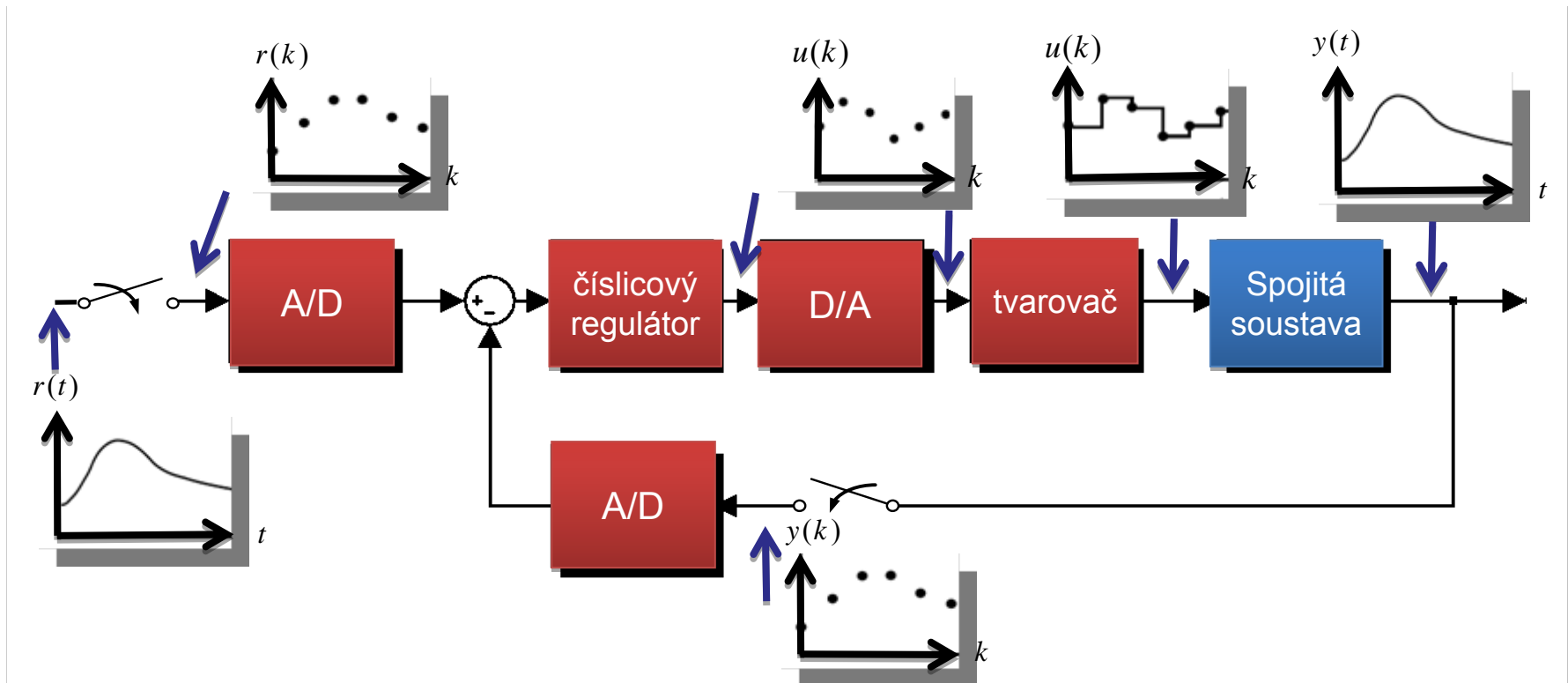
Discrete-time system & digital controller ...





Digital control & continuous-time systems

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-multi-rate sampling

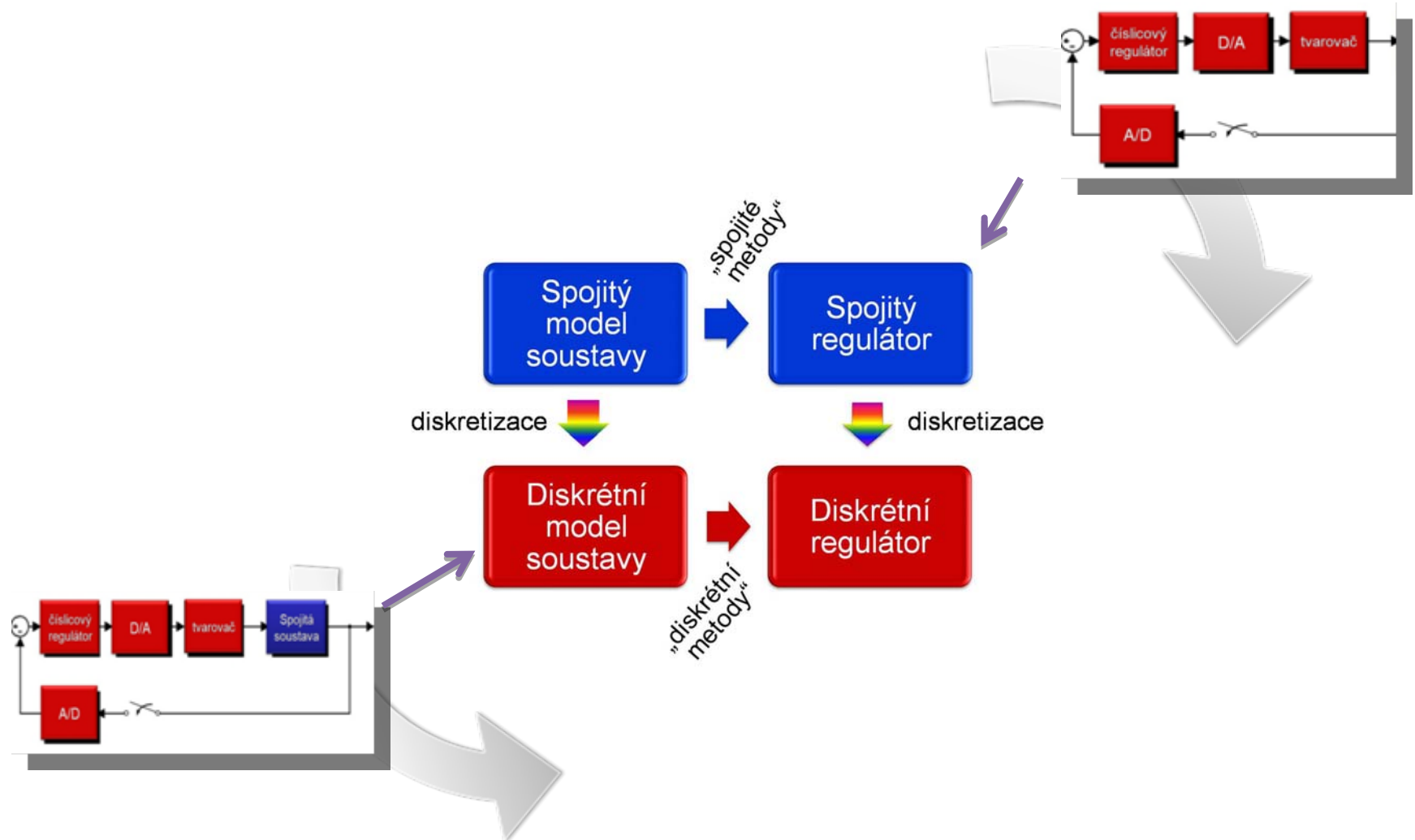
-hybrid systems (CT plant / DT controls)

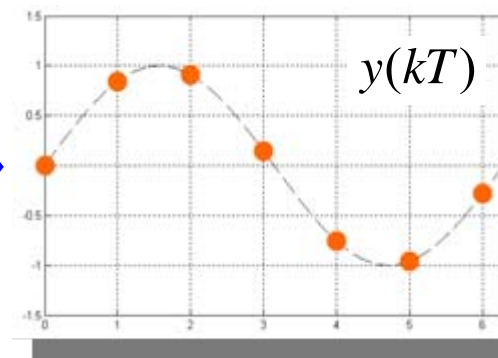
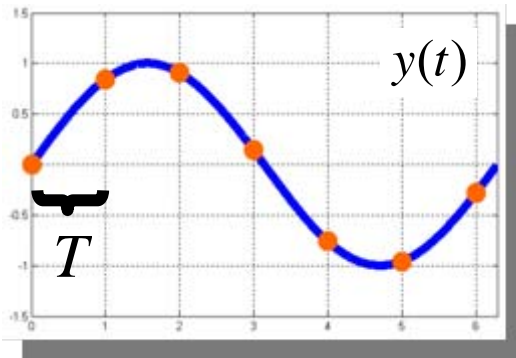
-event-driven sampling (batch-processes)

-...

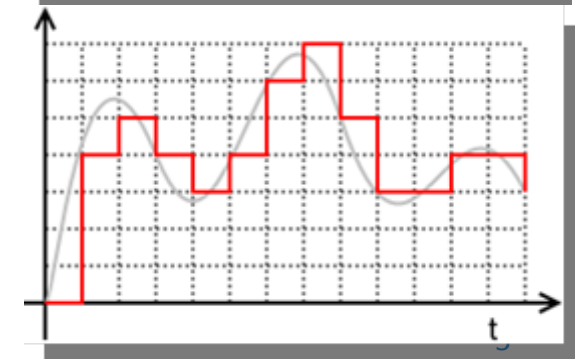
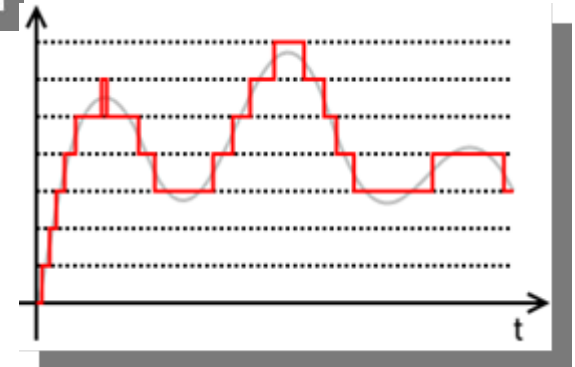


Design options for digital controllers





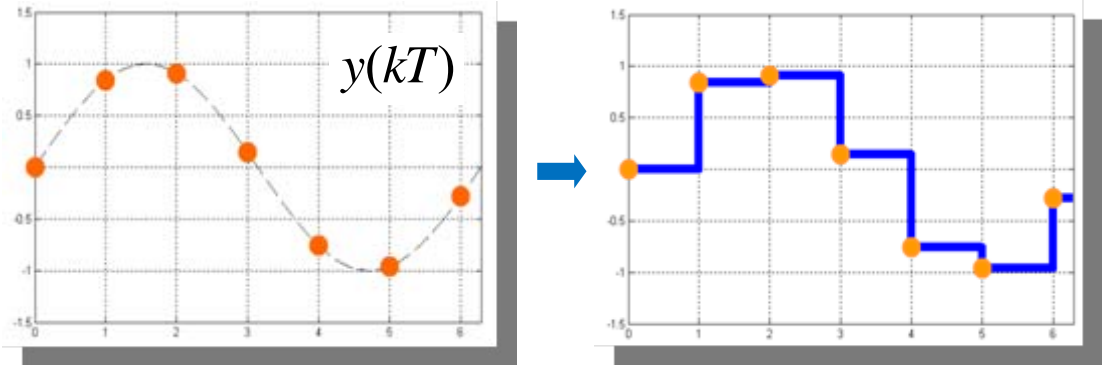
- quantization
- sampling
- digitization





Reconstruction

- reconstruction = holding
- zero-order hold (ZOH)
- $\frac{1}{2} T_s$ delay effect ...

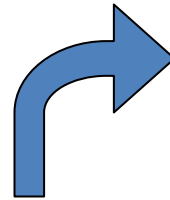
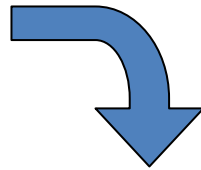




s and z variables relationship

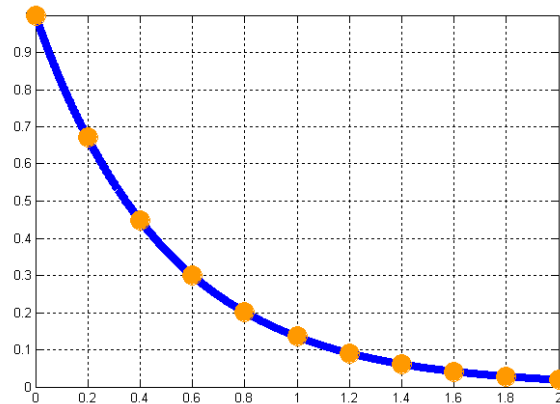
$$f(t) = e^{-at}, t > 0$$

$$F(s) = \mathcal{L}\{f\} = \frac{1}{s+a}$$



$$f(t) = e^{-akT}$$

$$F(z) = \mathcal{Z}\{f(kT)\} = \frac{z}{z - e^{-aT}}$$

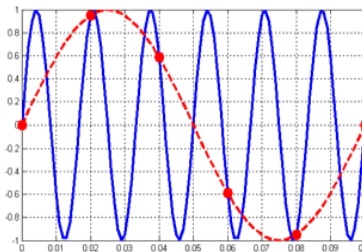


$$z = e^{sT}$$



Sampling theorem. Aliasing.

- Sampling theorem (Shannon, Nyquist, Kotělnikov,...)
- consequences: CD standard (44.1 kHz), ...
- aliasing (non-control examples: movies with rotating cars' wheels, digital pictures & moire, ...). Solution: anti-aliasing (=low-pass) filter.



$$\omega_s > 2\omega_{\max}$$

$$\omega_N = \omega_s / 2 = \pi / T_s > \omega_{\max}$$



Sampling frequency for control problems

-purely theoretical minimum:

$$\omega_S > 2\omega_{BW}$$

-practical usual solutions:

$$\omega_S > (20 \leftrightarrow 40) \times \omega_{BW}$$

-alternatively: 5-10 samples per rise-time

-simulation verification is “a must-do”

-Ts can range from microseconds (HD drives, audio/active damping applications) to tens-of-minutes/hours (chemical plants, process industry)

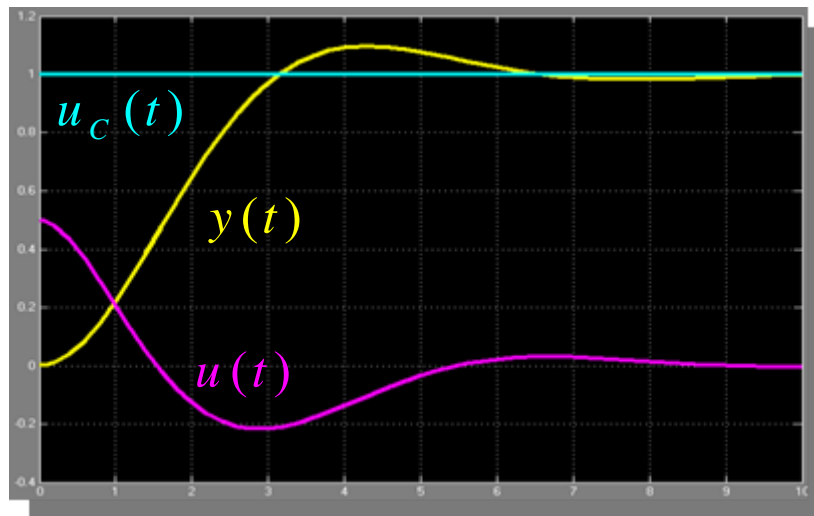
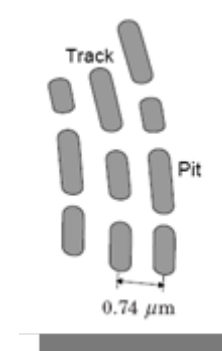
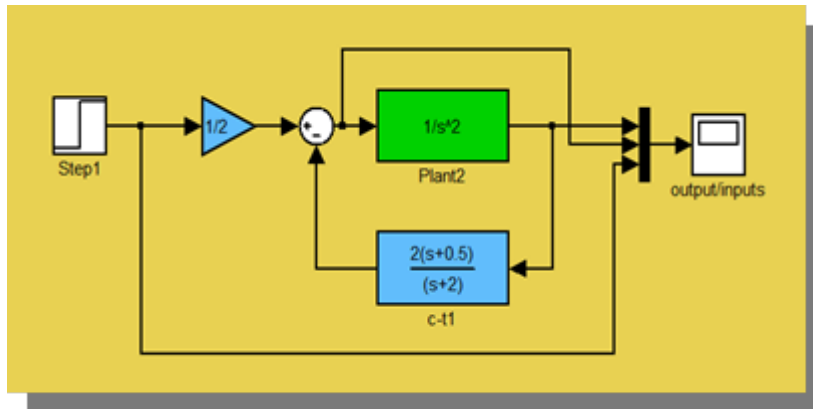
-sampling rates implies potential complexity of the control laws (hence e.g. MPC started in process controls)

mind: non-causal characteristics of ideal reconstructor.
Delay of higher-order holds (1st, 2nd order) unacceptable for controls typically.



Example (Astrom, Digital Control)

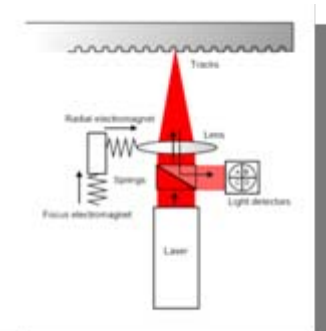
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- HD drive arm control / dynamics compensation

- by lead feedback 1st order controller

- the head is modelled as double integrator only





Example (Astrom, Digital Control)

$$u(s) = 0.5u_c(s) - 2 \frac{s + 0.5}{s + 2} y(s) = 0.5u_c(s) - 2y(s) + 2 \frac{1.5}{s + 2} y(s)$$
$$= 2 \left[0.25u_c(s) - y(s) + x(s) \right]$$

$$x(s) = \frac{1.5}{s + 2} y(s)$$

$$u(t) = 2 \left[0.25u_c(t) - y(t) + x(t) \right]$$

$$\frac{dx}{dt} = -2x(t) + 1.5y(t)$$

$$\frac{x(t+h) - x(t)}{h} = -2x(t) + 1.5y(t)$$


$$u(t_k) = 2 \left[0.25u_c(t_k) - y(t_k) + x(t_k) \right]$$
$$x(t_k + h) = x(t_k) + h \left[1.5y(t_k) - 2x(t_k) \right]$$



Example (Astrom, Digital Control)

$$u(t_k) = 2[0.25u_C(t_k) - y(t_k) + x(t_k)]$$

$$x(t_k + h) = x(t_k) + h[1.5y(t_k) - 2x(t_k)]$$



$$\frac{dx}{dt} \rightarrow \frac{x(t+h) - x(t)}{h}$$


$$u(t) = 2[0.25u_C(t) - y(t) + x(t)]$$

$$\frac{dx}{dt} = -2x(t) + 1.5y(t)$$

$$u(z) = 2[0.25u_C(z) - y(z) + x(z)]$$

$$zx(z) = x(z) + h[1.5y(z) - 2x(z)]$$

$$u(z) = 0.5u_C(z) - 2\frac{z + 0.5h - 1}{z + 2h - 1}y(z)$$



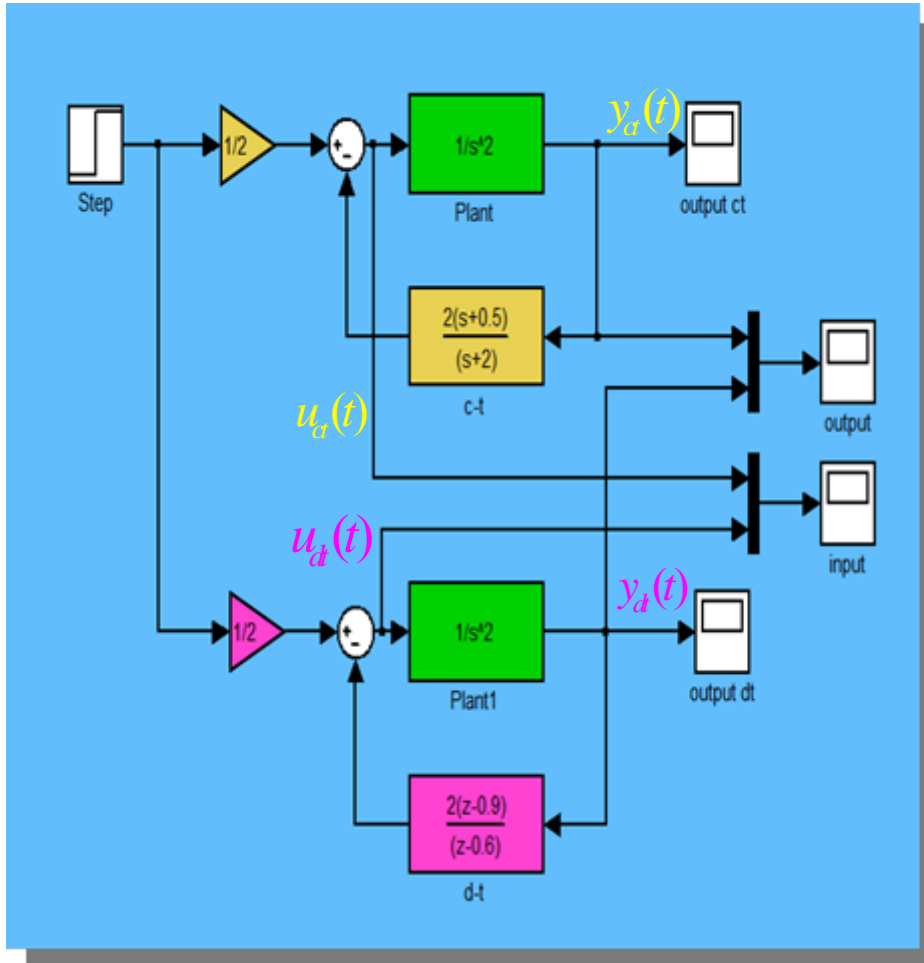
$$s \rightarrow \frac{z-1}{h}$$

$$u(s) = \frac{1}{2}u_C(s) - 2\frac{s + 0.5}{s + 2}y(s)$$



Example (Astrom, Digital Control)

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Example (Astrom, Digital Control)

- $h = 0.1, 0.5, 1, 1.5$

