

PROSTOROVĚ DISTRIBUOVANÉ SYSTÉMY (SYSTÉMY S ROZPROSTŘENÝMI PARAMETRY)

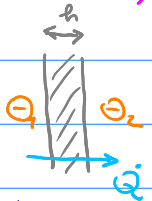
(A3B35MSD 2014/15)

TEPELNÉ SYSTÉMY

$$\dot{Q} = \frac{H}{\frac{A \cdot \lambda}{h}} (\Theta_1 - \Theta_2)$$

$h \rightarrow 0$:

$$\dot{Q} = -A \cdot \lambda \cdot \lim_{h \rightarrow 0} \frac{\Theta(x+h) - \Theta(x)}{h}$$



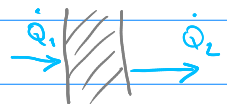
$$\frac{dQ(x,t)}{dt} = -A \cdot \lambda \cdot \frac{\partial}{\partial x} \Theta(x,t)$$

$$\dot{Q}_x = -k \cdot \Theta_x$$

... Fourier

$$Q = m \cdot c \cdot \Theta = \int \rho \cdot c \cdot \Theta dV$$

$$\dot{Q} = \frac{d}{dt} \int_a^b \rho c \Theta dx = \left[\int_a^b \rho c \dot{\Theta} dx \right] = \dot{Q}_1 - \dot{Q}_2$$



$$\begin{aligned} &= -(\dot{Q}_2 - \dot{Q}_1) \\ &= -(\dot{Q}(b) - \dot{Q}(a)) \\ &= - \int_a^b \frac{\partial \dot{Q}}{\partial x} dx + \int_a^b g(x,t) dx \end{aligned}$$

Obečně pro 3d:

$$-\oint_A (\dot{Q} \cdot n) dA$$

$$= - \int_V (\nabla \cdot \dot{Q}) dV$$

$$= - \int_V \nabla \cdot (-k \nabla \Theta) dV$$

$$\int_V \rho c \dot{\Theta} dV = \int_V k \nabla^2 \Theta dV$$

$$\int_a^b \rho c \dot{\Theta} dx = - \int_a^b \frac{\partial \dot{Q}}{\partial x} dx + \int_a^b g dx$$

$$\rho c \dot{\Theta} = - \frac{\partial}{\partial x} \left(-k \frac{\partial \Theta}{\partial x} \right) + g$$

$$\Theta_t - \frac{k}{\rho c} \cdot \Theta_{xx} = \frac{1}{\rho c} g$$

$$\Rightarrow \dot{\Theta} - \frac{k}{\rho c} \cdot \Delta \Theta = \frac{1}{\rho c} g$$

$$\Delta = \frac{\partial^2}{\partial x^2} + \frac{\partial^2}{\partial y^2} + \frac{\partial^2}{\partial z^2}$$

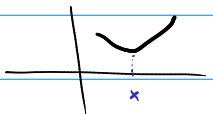
no heaters inside:

$$\boxed{\Theta_t = \alpha \cdot \Theta_{xx}} \quad \alpha > 0$$

či

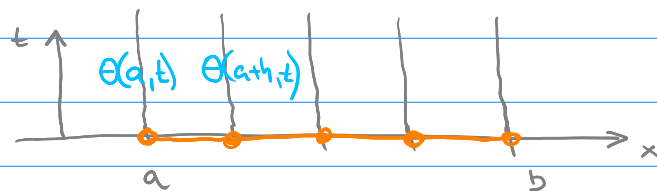
$$\boxed{\dot{\Theta} = \alpha \cdot \Delta \Theta}$$

... tepelná rovnice

Θ_{xx} kvantifikuje zakřivení: $\Theta_{xx} > 0 \Rightarrow$ 

V ustáleném stavu ($t \rightarrow \infty$): $\boxed{0 = \alpha \cdot \Theta_{xx}}$

Method of lines (MOL)



Místo $\Theta(x,t)$ použijeme

$$\begin{bmatrix} \Theta_1(t) \\ \Theta_2(t) \\ \vdots \\ \Theta_n(t) \end{bmatrix} \approx \begin{bmatrix} \Theta(a+h) \\ \Theta(a+2h) \\ \vdots \end{bmatrix} \quad \begin{cases} \Theta_0 := \Theta(a) \\ \Theta_{n+1} := \Theta(b) \end{cases}$$

Aproximace $\Delta \Theta$ (či v 1D: $\frac{\partial^2 \Theta}{\partial x^2}$)

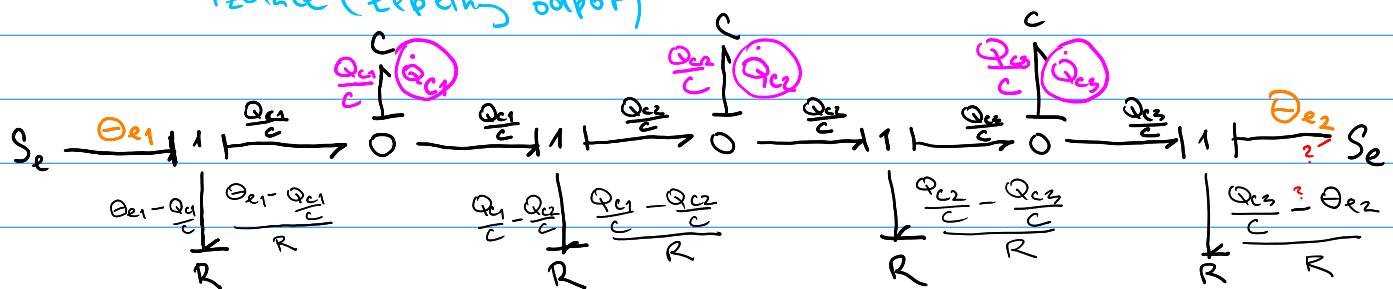
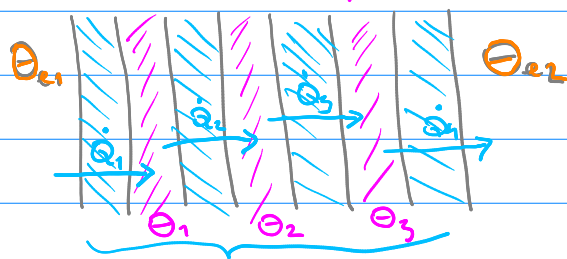
Centrální difference: $\frac{\partial \Theta}{\partial x} \approx \frac{\Theta(x + \frac{1}{2}h) - \Theta(x - \frac{1}{2}h)}{h}$

$$\frac{\partial^2 \Theta}{\partial x^2} \approx \frac{\frac{\Theta(x+h) - \Theta(x)}{h} - \frac{\Theta(x) - \Theta(x-h)}{h}}{h}$$

$$= \frac{1}{h^2} (\Theta(x+h) - 2\Theta(x) + \Theta(x-h))$$

$$\begin{bmatrix} \dot{\Theta}_1 \\ \dot{\Theta}_2 \\ \vdots \\ \dot{\Theta}_n \end{bmatrix} = \frac{\alpha}{h^2} \begin{bmatrix} \Theta_2 - 2\Theta_1 + \Theta_0 \\ \Theta_3 - 2\Theta_2 + \Theta_1 \\ \vdots \\ \Theta_{n+1} - 2\Theta_n + \Theta_{n-1} \end{bmatrix} = \frac{\alpha}{h^2} \begin{bmatrix} -2 & 1 & \dots & 0 \\ 1 & -2 & 1 & \dots \\ & \ddots & \ddots & \ddots \\ 0 & \dots & 1 & -2 \end{bmatrix} \begin{bmatrix} \Theta_1 \\ \Theta_2 \\ \vdots \\ \Theta_n \end{bmatrix} + \frac{\alpha}{h^2} \begin{bmatrix} 1 & 0 \\ 0 & 1 \\ \vdots & \vdots \\ 0 & 1 \end{bmatrix} \begin{bmatrix} \Theta_0 \\ \Theta_{n+1} \end{bmatrix}$$

Diskretizace pomocí vazebních grafů



$$\dot{Q}_{c1} = \frac{\Theta_{e1} - \frac{Q_{c1}}{C}}{R} - \frac{\frac{Q_{c1}}{C} - \frac{Q_{c2}}{C}}{R} = \frac{\Theta_{e1}}{R} - \frac{2 \cdot \frac{Q_{c1}}{C}}{R} + \frac{\frac{Q_{c2}}{C}}{R}$$

$$\dot{Q}_{c2} = \frac{\frac{Q_{c1}}{C}}{R} - \frac{2 \cdot \frac{Q_{c2}}{C}}{R} + \frac{\frac{Q_{c3}}{C}}{R}$$

$$\dot{Q}_{c3} = \frac{\frac{Q_{c2}}{C}}{R} - \frac{2 \cdot \frac{Q_{c3}}{C}}{R} + \frac{\Theta_{e2}}{R}$$

$$Q_c = \Theta_c \cdot C :$$

$$C \cdot \dot{\Theta}_{c1} = \frac{1}{R} \Theta_{e1} - 2 \cdot \frac{C \cdot \Theta_{c1}}{R} + \frac{C \cdot \Theta_{c2}}{R}$$

$$C \cdot \dot{\Theta}_{c2} = \frac{C \cdot \Theta_{c1}}{R} - 2 \cdot \frac{C \cdot \Theta_{c2}}{R} + \frac{C \cdot \Theta_{c3}}{R}$$

$$C \cdot \dot{\Theta}_{c3} = \frac{C \cdot \Theta_{c2}}{R} - 2 \cdot \frac{C \cdot \Theta_{c3}}{R} + \frac{1}{R} \Theta_{e2}$$

$$\begin{bmatrix} \dot{\Theta}_{c1} \\ \dot{\Theta}_{c2} \\ \dot{\Theta}_{c3} \end{bmatrix} = \frac{1}{R} \begin{bmatrix} -2 & 1 & 0 \\ 1 & -2 & 1 \\ 0 & 1 & -2 \end{bmatrix} \begin{bmatrix} \Theta_{c1} \\ \Theta_{c2} \\ \Theta_{c3} \end{bmatrix} + \begin{bmatrix} \frac{1}{R} & 0 \\ 0 & 0 \\ 0 & +\frac{1}{R} \end{bmatrix} \begin{bmatrix} \Theta_{e1} \\ \Theta_{e2} \end{bmatrix}$$

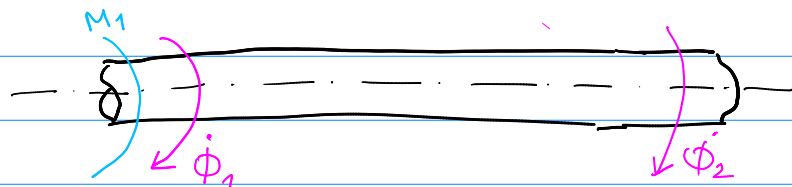
?? A ??

$$R = \frac{1}{H} = \frac{h}{A \cdot \gamma}$$

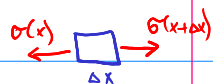
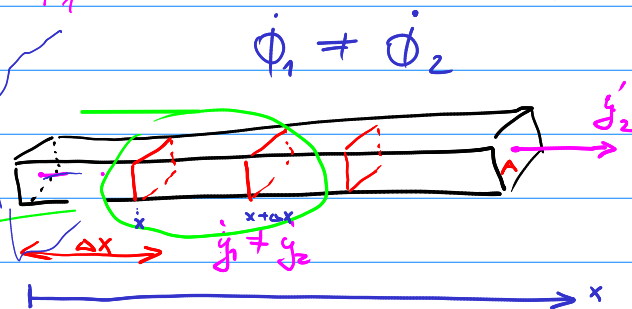
$$C = m \cdot c = A \cdot h \cdot \rho \cdot c$$

$$\frac{1}{R \cdot C} = \frac{A \cdot \gamma}{h \cdot A \cdot h \cdot \rho \cdot c} = \frac{\gamma}{\rho \cdot c} \cdot \frac{1}{h^2}$$

PRUŽNÁ HŘÍDEL



nebo polečné kmitání:



$$\underbrace{\Delta x \cdot A \cdot \rho}_{m} \cdot \ddot{y}(x,t) = A \cdot \underbrace{\sigma(x+\Delta x)}_{\text{STRESS}} - A \cdot \sigma(x)$$

směruje ven / : Δx, Δx → 0

$$A \rho \frac{\partial^2 y}{\partial t^2} = A \cdot \frac{\partial \sigma}{\partial x} \Rightarrow \frac{\partial^2 y}{\partial t^2} = \frac{1}{\rho} \frac{\partial \sigma}{\partial x}$$



STRAIN = RELATIVE DEFORMATION

$$\sigma(x,t) = E \cdot \frac{y(x) - y(x-\Delta x, t)}{\Delta x}$$

Young

Δx → 0

$$\sigma = E \cdot \frac{\partial y}{\partial x}$$

$$\frac{\partial^2 y}{\partial t^2} = \frac{E}{\rho} \frac{\partial^2 y}{\partial x^2}$$

$$\frac{\partial^2 y}{\partial t^2} = c^2 \frac{\partial^2 y}{\partial x^2}$$

... VLNOVÁ ROVNICE

c... rychlost šíření vlny

$$m \cdot \ddot{y} =: p$$

⇒ 1. rovnice:

$$\dot{\Phi} = F(x+\Delta x) - F(x)$$

$$\Rightarrow \dot{\Phi}_k = F_{k+1} - F_k$$

2. rovnice:

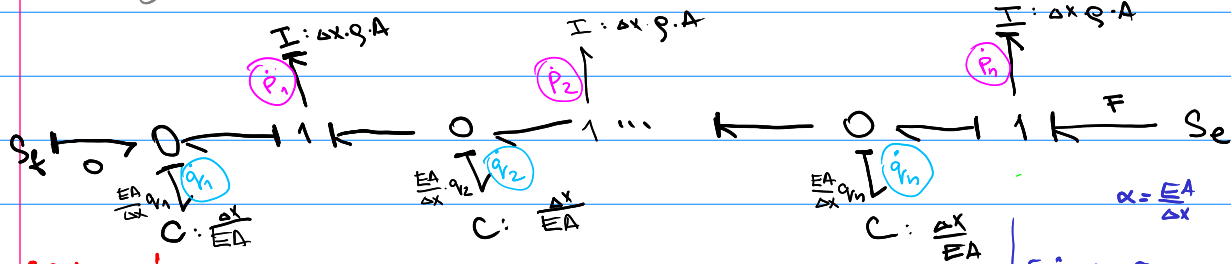
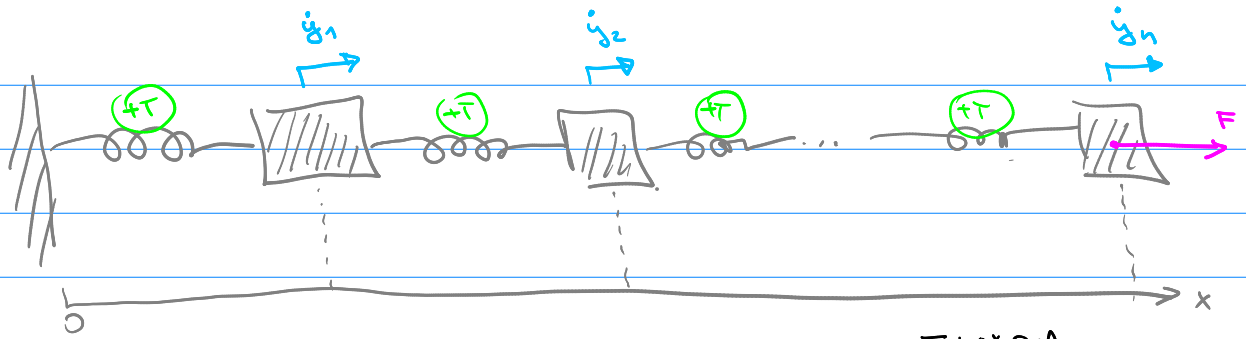
$$F(x) = \frac{EA}{\Delta x} \cdot q(x)$$

$$q = y(x) - y(x-\Delta x)$$

$$F_k = \frac{EA}{\Delta x} \cdot q_k$$

$$\dot{\Phi}_k = \frac{EA}{\Delta x} (q_{k+1} - q_k)$$

$$\dot{q}_k = \dot{y}(x) - \dot{y}(x-\Delta x) = \frac{(p_k - p_{k-1})}{\Delta x \cdot \rho \cdot A}$$



$$\alpha = \frac{EA}{\Delta x} \quad \beta = \frac{1}{\Delta x \rho A}$$

PRVNÍ A POSLEDNÍ:

$$\dot{q}_1 = \frac{1}{\Delta x \rho A} \cdot P_1$$

$$\dot{p}_n = F - \frac{EA}{\Delta x} q_n$$

$$\dot{P}_k = \frac{EA}{\Delta x} (q_{k+1} - q_k)$$

$$\dot{q}_k = \frac{(P_k - P_{k-1})}{\Delta x \rho A}$$

$$\Downarrow \Delta x \rightarrow 0$$

$$\frac{\partial P}{\partial t} = EA \frac{\partial q}{\partial x}$$

$$\Downarrow \Delta x \rightarrow 0$$

$$\frac{\partial q}{\partial t} = \frac{1}{\rho A} \cdot \frac{\partial P}{\partial x}$$

$$\begin{bmatrix} \frac{\partial P}{\partial t} \\ \frac{\partial q}{\partial t} \end{bmatrix} = \begin{bmatrix} 0 & EA \frac{\partial}{\partial x} \\ \frac{1}{\rho A} \frac{\partial}{\partial x} & 0 \end{bmatrix} \cdot \begin{bmatrix} P \\ q \end{bmatrix}$$

$$\begin{bmatrix} \dot{P}_1 \\ \dot{P}_2 \\ \vdots \\ \dot{P}_n \\ \dot{q}_1 \\ \dot{q}_2 \\ \vdots \\ \dot{q}_n \end{bmatrix} = \begin{bmatrix} \alpha & \alpha & 0 & 0 \\ & -\alpha & \alpha & 0 \\ & & \ddots & \ddots \\ & & & -\alpha & \alpha \\ & & & & 0 \\ & \beta & & & \\ & & \beta & & \\ & & & \beta & \\ & & & & \beta \end{bmatrix} \begin{bmatrix} P_1 \\ P_2 \\ \vdots \\ P_n \\ q_1 \\ q_2 \\ \vdots \\ q_n \end{bmatrix}$$

$$+ \begin{bmatrix} 1 \\ \vdots \\ 1 \end{bmatrix} \cdot F$$

$$\begin{bmatrix} \dot{y}_1 \\ \dot{y}_2 \\ \vdots \\ \dot{y}_n \end{bmatrix} = \begin{bmatrix} 1 & & & \\ & 1 & & \\ & & \ddots & \\ & & & 1 \end{bmatrix} \begin{bmatrix} q_1 \\ q_2 \\ \vdots \\ q_n \end{bmatrix}$$

ALSO TAKE:

$$v = \dot{y}$$

$$\begin{bmatrix} \frac{\partial y}{\partial t} \\ \frac{\partial v}{\partial t} \end{bmatrix} = \begin{bmatrix} 0 & 1 \\ \frac{E}{\rho} \frac{\partial}{\partial x} & 0 \end{bmatrix} \cdot \begin{bmatrix} y \\ v \end{bmatrix}$$

$$\begin{aligned} q_1 &= y_1 \\ q_2 &= y_2 - y_1 \\ q_3 &= y_3 - y_2 \\ q_k &= y_k - y_{k-1} \\ q_n &= y_n - y_{n-1} \end{aligned}$$

✓ VĚDY UPŘESNIT OKRAJOVÉ A POČÁTEČNÍ PODMÍNKY